Performace Evaluation & Life Cycle Costs In Rewound Induction Motors Used In Spinning Units

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Abstract: Induction motors being the major energy consumer in the plant offer opportunities of energy saving. In the spinning unit many induction motors are in-house rewound. This paper reports the analysis done on the rewound induction motors to determine its efficiency and life cycle cost comparison. Practical comparisons between rewound motors and the new motors are shown.

Keywords: Rewound induction motor, energy loss, efficiency, life cycle cost, spinning unit.

I. INTRODUCTION

The electrical motors consume large amount of electrical energy. Nearly 80-85% of the load in a spinning unit is on account of induction motors [1]. In these industries a common prevalent practice is to repair and rewind a faulty motor, instead of replacing it with a new one. The efficiency of the motor decreases after it is rewound. This short term capital saving method thus may have a huge long term loss.

II. PROBLEM DEFINITION

The rewound induction motors in textile plant under study are to be analysis for different types of losses in order to get their overall efficiency. The efficiencies of all these motors are then to be compared with the rated and actual efficiencies of new motors taking replacement as one of the options. Recommendations for replacement of rewound motors are to be made accordingly.

III. METHOD

Many in-house rewound induction motors are identified in a major textile plant after several visits. Working condition of each in-house rewound induction motor is examined. All the parameters of the rewound induction motors are identified and recorded through different means. All the parameters are divided into three different types i.e. rated, measured and calculated. Different instruments are used to measure the measurable parameters that lead to determination of its efficiency [2]. The parameters and respective instruments used in this exercise are listed in the Table 1.

Parameter	Instrument			
Speed	Tachometer			
Current	Clamp-on-transducer			
Voltage	Power analyzer			
Input power Winding	Power analyzer			
temperature	Resistance temp. detector			
Winding resistance	Power analyzer			

Table 1							
Parameters	and	Instruments	Used				

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Figure 1: Procedure to Analysis of the Motor

IV. RESULTS AND DISCUSSION

In the plant, the saving in electrical energy is found by analyzing some of the in-house rewound induction motors and looking for alternative options to increase the efficiency of the motors. Sample parameters of one of the in-house rewound induction motor are given in Table 2 after applying the relevant formulae [3, 4].

Table 2 Rated and Measured Parameters of Rewound Induction Motor

Parameters	Measured Parameters				
No. of phases, f	3 No-load voltage, <u>VNa-load</u> (V) 410				
No. of poles, p	4 No-load current, JNg-load (A) 10				
Power, P _{rated}	No-load input power, P _{No-load}				
(HP)	20 (W) 660				
	Winding Temp. of still motor,				
Voltage, V _{ated} (V)	415 T1 (°C) 24				
	Resistance at room temp., R1				
Current, L _{avei} (A)	27 (W) 1.2				
Full-load speed,	Winding Temp. of no-load 1460 motor, 41				
	(°C)				
N _{rated} (RPM) Supply	Winding Temp. of loaded				
frequency,	50 motor(⁰ c), 141				
f (Hz)					
_	 Full-load voltage (V) 410 				
_	- Full-load current, IFull-load (A) 31				
	Full-load i/p power, PEull-load				
_	- (W) 17300				
_	- Full-load speed, N2 (RPM) 1475				
_	- No-load speed, N1 (RPM) 1490				
ynchronous spe	ed				
Calculated param synchronous spec- Ns = $(120 \text{ X f}) / P$ Stator resistance a $R = R_0 (1+\alpha t) =$ Stator resistance a	ed =120x50/4=1500 rpm at no load =1.05 Ω				
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Determined efficiency of an analyzed in-house rewound induction motor = 84.2 % Similarly, determined efficiency of an analyzed new motor = 93.25 % Analysis done on few rewound motors including described above is shown below in the form of graphs:



Figure 3: 20HP Motor Analysis



Figure- 4: 50HPMotor Analysis

Figure 2-4 show the efficiencies of new and rewound motors thus rewound motors has low efficiency and more losses. [5].

Life Cycle Cost of Induction Motor

The majority of motors in the field are induction motors. The industry is becoming increasingly concerned about the ability of electric motors to ride through power system disturbances. There may be various reasons for the desire of testing induction motors in the field, such as the consideration of exchanging out of date or worn motors with new, or checking the efficiencies after rewinding.

Life Cycle Cost Comparison of Induction Motor

Indian industry is currently feeling a squeeze on profits due to the rapid rise in power costs. It is no longer practical to consider the monthly power bill as a fixed base cost that cannot be controlled. Power costs have been raising faster than both material and producer good prices. During the 2000's they were increasing at approximately the same rate, and it was generally possible to pass any power increase along to the customer in the form of a price increase. After the energy crunch, power rates increased much faster than the prices for products, so any portion of power posts that could not be passed along came directly out of profits. Since motors account for over 90 percent of power used by industry, they have always had an impact on operating costs. In today's economy, it is more important than ever to keep the cost of motor losses under control. So for Life cycle cost comparison method first of all we have to calculate the rated speed, Efficiencies, Prices of new and rewind motors.

Life-Cycle Cost (LCC) LCC=PP + $EF \times K W_e$ here LCC= Life Cycle Cost PP= Motor Purchase price EF= Evaluation Factor KW_e = Evaluated loss.

Motor type and Rating	Life Cycle Cost of One Year(Rupee)						
	New	R.M 1	R.M 2	R.M 3	R.M 4	R.M 5	
15HP	237694	299950	319241	280328	429935	313857	
20HP	316342	504720	488797	449082	568183	461160	
50HP	555819	1153253	1339678	1539806	992819	1198337	

Table-3 Life cycle cost comparison of different motors

V. CONCLUSION AND FUTURE SCOPE

In spinning unit many induction motors are reused after rebounding. In the present study, performance evaluation and efficiency analysis of rewound motors has been done and the results are compared with those of new motors. Also life cycle costs of new and rewound motors have been evaluated and compared. From the study, it is found that rewound motor consumes 1.5 times to 3 times more energy than new motor Based on the study recommendation has been suggested. Scope of power saving exists in improving the power-factor. A future study on power factor analysis and improvement in thus suggested.

REFERENCE:

- [1]. Cummings Paul G, Bowers W. D, "Induction Motor Efficiency Test Methods", IEEE Transactions On Industry Applications, VOL. IA-17, No. 3, May/June 1981, PP 253-272
- [2]. Aquila A. Dell', Salvatore L., and Savino M. "A New Test Method for Determination of Induction Motor Efficiency IEEE Power Engineering Review, October 1984, PP 48-49
- [3]. Montgomery David C, "The Motor Rewind Issue-A New Look", IEEE Transactions on Industry Applications, VOL. LA-20, NO. 5, September/October 1984, PP 1330-1336
- [4]. Schwartz Thomas F., Discussion of "The Motor Rewind Issue- A New Look", IEEE Transactions on Industry Applications. VOL IA-21, NO.2.. March/April 1985, PP 356
- [5]. Richter Eike, MillerTimothy J.E, Neumann Thomas W, Hudson Thomas L, "The Ferrite Permanent Magnet AC Motor-A Technical and Economical Assessment", IEEE Transactions on Industry Applications, VOL. IA-21, NO. 4, May/June 1985, PP 644-650
- [6]. Binns D.F., "Comparative costs of energy losses in induction Motors", Electric Power Application IEEE Proceedings, Vol. 134, Pt. B, No. 4, July 1987, PP 177-182
- [7]. Medarametla J. B, Cox M. D, Baghzouz Y, "Calculations And Measurements Of The Unity Plus Three-Phase Induction Motor", IEEE Transactions on Energy Conversion, Vol. 7, No 4, December 1992, PP732-738
- [8]. Grantham C, McKinnon D.J, "A Novel Method for Load Testing and Efficiency Measurement of Three-phase Induction Motors", Electric Machines and Drives Conference IEEE, IEMDC'03. IEEE International, 2003, PP769-775
- [9]. Hamer Paul S, Lowe Debra M, Wallace Stanley E, "Energy-Efficient Induction Motors Performance Characteristics and Life-Cycle Cost Comparisons for Centrifugal Loads", IEEE Transactions on Industry Applications, VOL. 33, NO. 5, September/October 1997, PP 1312-1320
- [10]. Hsu J. S, Kueck J. D, Olszewski M, Casada D. A, Otaduy P. J, Tolbert L. M, "Comparison of Induction Motor Field Efficiency Evaluation Methods", Industry Applications Conference, 1996, Thirty First IAS Annual Meeting, IAS'96., Conference Record of the 1996 IEEE, vol. 1, PP 703-712