# Study on the change of porosity and permeability of sandstone reservoir after water flooding

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**Abstract:** After water flooding development, Great changes have occurred in the porosity and permeability of sandstone reservoirs with the development time. The value of these parameters will effect reserves calculation and numerical simulation, and have an important role of guiding development adjustment programs and tapping remaining oil. In this paper, the varieties of reservoir parameters were analyzed with the results of logging interpretation and core analyzing. The values of porosity and permeability gradually increased with the development time. There exists four period during the whole stage: platform period, slow ascent period, fast rising period and relatively stable period. It is mainly related to the formation process of the underground seepage network. The change of porosity and permeability is mainly affected by reservoir properties, water injection time and well density. The better the original physical property of the reservoir, the longer the injection time and the greater the density of well network, then variation of porosity and permeability is larger. When the well spacing density reach 50-60 well/km<sup>2</sup> and average water saturation is about 55 percent, reservoir porosity and permeability will not increase obviously.

#### Keywords: Reservoir; Porosity; Permeability; Water saturation; Well density

The research results at present show that the porosity and permeability of the reservoir have changed to a different degree with the increase of the oil field exploitation time. Especially in the heterogeneous reservoirs, Long-term water injection leads to the formation of the preponderance flow path. there is different water-injected multiple in different location, so porosity and permeability changes are different. Furthermore, the reservoir heterogeneity is further exacerbated. It will directly affect the distribution of the remaining oil in oilfields. Therefore, it has important significance to grasp the rules of the variation of porosity, permeability with time was studied with the data of cores and well logging in Xingshugang oilfield Sapu oil layer, and the reasons leading to the changes were analyzed.

Xingshugang oilfield is located in the Heilongjiang Province, Daqing City. The reservoir of SA Pu layer buried depth is 1000m around, Reservoir was formed in fluvial delta depositional environment, there mainly developed sand bodies such as meandering river, delta distributary plain, delta front and prodelta during the period.

The target area began to be developed from the 1960s and has experienced four well network period till today: The basic well pattern (1960-1983), the first well pattern (1984-1993), the second well pattern (1994 to 2006), the third well pattern (2007-2015). Because the data of drilling, logging and cores can be reflected the characteristics of the reservoir parameters in different time, the variation of reservoir parameters during different periods can be analyzed using these data.

#### I. THE CHANGE OF POROSITY AND PERMEABILITY OF RESERVOIR AFTER WATER FLOODING

With the data of porosity and permeability value from different core wells in different time, after water flooding, The average porosity is generally increased by 0.5-4% and the average permeability is increased unequal  $100-600 \times 10^{-3} \mu m^2$ . The porosity and permeability changes of different sand body were different. In target area, The types of sand body is rich affected by depositional environment, to comprehensively study different sand bodies porosity and permeability variations during the period of water flooring, porosity and permeability of different samples were analyzed. These samples are from sand bodies in different depositional environment, they include Meandering river sand bodies, overwater channel sand bodies, submerged channel sand bodies, overwater non channel sand bodies and submerged non channel sand bodies. The changes of porosity and permeability of these sand bodies were analyzed by using 5 core wells (Table 1).

| Table 1 The change of porosity and permeability of different said bodies before and after water moduling |           |              |       |      |   |         |        |  |  |
|--|-----------|--------------|-------|------|---|---------|--------|--|--|
| Sand body types  | Thickness | Porosity (%) |       |      | Permeability $(\times 10^{-3} \mu m^2)$ |         |        |  |  |
|  | (m)       | before       | after | rise | before                                  | after   | rise   |  |  |
| Meandering river   | 6.7       | 28.41        | 31.68 | 3.27 | 909.42                                  | 1470.1  | 560.68 |  |  |
| Overwater channel  | 3.9       | 28.24        | 30.32 | 2.08 | 755.71                                  | 1002.45 | 246.74 |  |  |
| Submerged channel  | 3.2       | 28.26        | 28.54 | 0.28 | 407.42                                  | 659.21  | 251.79 |  |  |
| Overwater non channel  | 0.9       | 27.96        | 28.1  | 0.14 | 354.25                                  | 548.04  | 193.79 |  |  |
| Submerged non channel  | 0.6       | 26.05        | 26.72 | 0.67 | 141.98                                  | 304.38  | 162.4  |  |  |

Table 1 The change of porosity and permeability of different sand bodies before and after water flooding

From the table 1, porosity and permeability of different sand bodies are increased with the increase of water injection time, but the increasing extent was different. The greater the thickness of the single sand bodies, the greater the increase in porosity and permeability. so the thickness of sand body in a certain extent can reflect the formation of sand bodies. The relation of porosity, permeability and thickness of single sand body were analyzed with the data from core wells in different periods, the results show that porosity and thickness, permeability and thickness have positive correlation. There exists different porosity and permeability change trend with different thickness: when thickness is greater than 2m, the change of porosity and permeability are little with thickness increase; when the thickness is in the range of 1-2m, there exist a middle porosity and permeability are greater with thickness of single sand body is greater than 2m), type II (the thickness of single sand body is greater than 1m).



Fig. 1 the cross-plot of porosity, permeability and the thickness of the single sand body

Porosity and permeability of all wells every year in target area were computed and counted, the porosity and permeability of different type sand bodies changed with time (Fig. 2).

(1) The porosity and permeability of different type sand bodies showed an upward trend, and the greater the thickness of the single sand body, the greater the rise.

The rise of type I sand bodies increased the maximum, the average porosity increased from 26.1% to 30.1%, the average penetration increased from  $447 \times 10^{-3} \mu m^2$  to  $102 \times 10^{-3} \mu m^2$ .

The rise of type II sand bodies was in the middle, the average porosity increased from 25.9% to 28.9%, the average penetration increased from  $293 \times 10^{-3} \mu m^2$  to  $61 \times 10^{-3} \mu m^2$ .

The rise of type III sand bodies is the smallest, the average porosity increased from 25.8% to 28.1%, and the average permeability increased from  $60 \times 10^{-3} \mu m^2$  to  $178 \times 10^{-3} \mu m^2$ .

(2) Porosity and permeability distribution area can be mainly divided into four sections according to the upward trend: the platform period before 1978, rapid rise period between 1979-1993, slowly rising period between 1994-2005 and relatively stable period after 2007.



Fig.2 The scatter plots of porosity, permeability and well density of different type sand bodies with time

The platform period before 1978: During this period, underground seepage field were forming, Interconnected pore throat network is in the formation stage. Average water saturation is less than 35% in the target area and average porosity and permeability keep no change.

Rapid rise period between 1979-1993: During this period, the change of reservoir parameters is relatively large. Porosity of type I sand bodies increased by 2.5% and the permeability increased by about  $165 \times 10^{-3} \mu m^2$ . Porosity of type II sand bodies increased by only 2% and the permeability increased by about  $87.6 \times 10^{-3} \mu m^2$ . Porosity of type III sand bodies increased by only 1.3% and permeability increased by about  $45.3 \times 10^{-3} \mu m^2$  In this stage, average water saturation in target area is always between 35-50%.

Slowly rising period between 1994-2005: During this period, the reservoir parameters change is slightly, Porosity of type I sand bodies increased by 1.2% and the permeability increased by about  $74.2 \times 10^{-3} \mu m^2$ . Porosity of type II sand bodies increased by only 0.9% and the permeability increased by about  $55 \times 10^{-3} \mu m^2$ . Porosity of type III sand bodies increased by only 0.6% and the permeability increased by about  $30.5 \times 10^{-3} \mu m^2$ . In this stage, average water saturation in target area is always between 50-55%.

Relatively stable period after 2007: During this period, the change trend of reservoir parameters is not obvious. At this time, the average water saturation in the area is more than 55%.

# II. THE INFLUENCE FACTORS OF RESERVOIR PARAMETERS CHANGE IN DIFFERENT PERIODS

It is considered that the change of reservoir parameters is mainly due to the migration of fine particles in the reservoir such as matrix and clay minerals, the change of the supporting mode among the particles and the distribution of pore throat size and so on. And these changes belongs to micro characteristic, they are mainly affected by the macro factors: Physical property of sand body, water injection time and well density.

#### (1) The effect of sand body physical property

As shown in Figure 2, the change of porosity, permeability of type I sand body is the greatest and the change of type III sand body is the smallest. Through the laboratory analysis data of 5 core wells, the main parameters of these kinds of sand bodies were obtained in Table 2. The particles size and distribution of different sand bodies are different, so the size and distribution of pore throats are different. This is mainly due to the

different hydrodynamic conditions in different depositional environment; there are greater particle size, thickness and better physical property in the sand bodies formed under high energy strong hydrodynamic environment. Conversely, there are smaller particle size, thickness and worse physical property in the sand bodies formed under low energy hydrodynamic environment.

| Sand body type | Particle size (mm) | Average pore<br>diameter (µm) | Porosity<br>(%) | Permeability $(\times 10^{-3} \mu m^2)$ |
|----------------|--------------------|-------------------------------|-----------------|---|
| Туре І         | 0.16               | 11.52                         | 30.05           | 1189.76                                 |
| Type II        | 0.12               | 7.77                          | 28.41           | 633.32                                  |
| Type III       | 0.07               | 5.16                          | 26.39           | 223.18                                  |

Table 2 Main properties of different sand bodies

The differences of physical properties of different sand bodies are mainly caused by the diameters of the pore throat, In the process of water injection development, the fluid flow in the reservoir pore throats follow Poiseuille Law. Flow velocities ( $\nu$ ) of single-phase liquid in capillary can be expressed as:

$$v = \frac{r^2 \Delta p}{8 \,\mu L}$$

In the formula: v: velocity,  $\mu$ m/s; r: pore diameter,  $\mu$ m;  $\Delta p$ : capillary pressure, Pa;  $\mu$ :fluid viscosity, pa·s; L: capillary length , $\mu$ m.

In the same pressure difference, the same channel length and the same fluid conditions, the flow rate(v) of fluid mainly depends on the pore diameter(r). If there are two equal length channels, the diameters is R1 and R2 respectively, and r1>r2. The ratio of the flow rate in the two channels is:

$$\frac{v_1}{v_2} = \left(\frac{r_1}{r_2}\right)^2$$

Then v1>v2, it showed that the faster the flow rate in the large pores. Due to water flooding front is actually composed of pores of different sizes, the velocity in large pore throat is much faster than in the little pore throat, Therefore, there are much more current quantity in large pore throat than in the little pore throat, the scouring action in large pore throat is more stronger. At the same time, fine particles of sand bodies can be flow out of reservoirs more easily along large pore throat, which leads to the increasing of porosity and permeability. Therefore, the greater the grain size, the greater the porosity and permeability, the stronger the effect of water injection on the porosity and permeability.



Figure 3 the scatter plot of particle number in displacement liquid and injection multiples

(2) The effect of water injection time

From Figure 2, with the increase of water injection time, the value of porosity and permeability increased gradually. But the change range is different in different period.

When oilfield is in the basic well pattern period, Underground seepage network were forming. During this stage, the injection water has not full of all pore throat networks, injection water is mainly used for filling new injection pore throat networks. Thus, the porosity and permeability value remain relatively constant, that is porosity and permeability platform period.

If well injection-production relationship remained unchanged for a long time, underground seepage network has formed, with the increase of injection time, injection multiples is also increase, especially in large pores, flow

velocity of the fluid is more faster, the particles in the pores are migrated easily, the rise of porosity and permeability is more higher.

Through water flooding scouring experiment with cores, the particles number is observed using Laser particle counter, The experimental results were shown in Figure 3, with the increase of injection time, the number of migrated particles present a first more and then few change trend, therefore with water flooding time increased, the rise of porosity and permeability are also showed a trend of first fast and then slow change trend.

#### (3) The influence of the well density

From Figure 2, there is good relevance between porosity, permeability and well density. The larger the well spacing density, the more the porosity and permeability increase.

It is mainly due to the increase of the number of the effective directions of single well, and the increase of the scope of water injection. As shown in Figure 4, without considering the type of sand body connectivity, the number of the effective direction of single well is 2 in the original well pattern(Fig.4-a), while the number of the average effective direction of single well is up to 2.5 after well pattern infilling(Fig.4-b). The fact shows that: the number of water channels is increased, swept volume of water injection is expand, the scope of water transformation is increased, so more particles migrated out of the underground, that leads to porosity and permeability of reservoirs increase intensified.



Fig. 4 Schematic diagram of the single well effectFidirection in the condition of different well density

### Fig. 5 the scatter plot of well density and water saturation

However, the increase of porosity and permeability will not last with the increase of well density, but there is a limitation. The statistics of the relationship between well density and water saturation, the result can be shown in Figure 5, with the increase of well density, water saturation increases, when the well density reach 50-60 well /  $km^2$ , Water saturation is no longer increased. The well spacing is about 200-250m. Even if the density of well

#### **III. CONCLUSION**

In this paper, the variation of reservoir parameters after water flooding is analyzed by means of logging interpretation and core analyzing. The following results are obtained:

(1)The porosity and permeability increased with the increasing of development time.

pattern is increased, the porosity and permeability will not increase obviously.

(2)The change of porosity, permeability is not uniform. It can be divided into four stages, which are the platform period, the fast rising period, the slow rising period and the relatively stable period. The phenomenon is mainly related to the formation process of the underground seepage network.

(3) the change of property and permeability is mainly affected by the sand body properties, the length of water injection time and well density. The better the original physical property of the reservoir, the longer the injection time and the greater the density of well network, then variation of porosity and permeability is larger. When the well spacing densities reach 50-60 well/km<sup>2</sup> and average water saturation is about 55 percent. Underground seepage network is relatively fixed, the porosity and permeability will not increase obviously.

#### REFERENCE

- [1] Song Wanchao, Sun Huanquan, Sun Guo, et a.l. Dynamical geologic process of development liquid—taking Shengtuo Oilfield as an example[J]. Acta Petrolei Sinica, 2003, 23(3): 52-55.
- [2] LI Cungui, Xu Shouyu. Law of pore structure verity in reservoir during a long episode water flooded development [J]. Petroleum Exploration and Development, 2003, 30(2):94-96.
- [3] Zhang Hongxing, Liu Qingnan, Li Fengqin. Variations of Petro physical parameters after sandstone reservoirs watered out in Daqing Oil Field [J]. SPE: 30884, 1995
- [4] P.Behrenbruch, H.M.Goda. Two-Phase Relative Permeability Prediction: A Comparison of the Modified Brooks-Corey Methodology with a New Carman-Kozeny Based Flow Formulation [J]. SPE: 101150, 2006
- [5] Han Jie, Song xinmin, Li Jun, et a.l. Experimental Research on the Changes in Formation Parameters during Water Flooding for Oil Production in Fuyu oilfield[J].Science Technology and Engineering, 2013,13(14): 3846-3850.