

PART-D EXP:1 (a)

S. No.	Temperature of oil in $^{\circ}\text{C}$.	observation.
1.	36 $^{\circ}\text{C}$	No change.
2.	56 $^{\circ}\text{C}$	No change.
3.	86 $^{\circ}\text{C}$	No change.
4.	106 $^{\circ}\text{C}$	No change.
5.	126 $^{\circ}\text{C}$	No change.
6.	156 $^{\circ}\text{C}$	No change.
7.	186 $^{\circ}\text{C}$	No change.
8.	190 $^{\circ}\text{C}$	No change.
9.	210 $^{\circ}\text{C}$	Flash Point
10.	240 $^{\circ}\text{C}$	Fire Point.

PART-A EXPT-1(b)

Observation and Tabulation:-

S No.	Temperature of oil °C	Observation
1.	36°C	No change.
2.	40°C	No change.
3.	66°C	No change.
4.	86°C	No change.
5.	106°C	No change.
6.	126°C	No change.
7.	156°C	No change.
8.	160°C	No change.
9.	170°C	No change.
10.	210°C	No change. Flash Point Fire Point No change

PART-A EXP. 2

Observation and Tabulation:-

- 1) Room temperature $T_R = 35^\circ\text{C}$
- 2) Density of oil at room temperature $0.85 \frac{\text{gm}}{\text{cm}^3}$

S. No.	Temperature of oil $^\circ\text{C}$.	Time taken of fill 50ml Flask in 'sec'	Kinematic viscosity in 'centi Stokes'	Density of oil gm/cm^3 .	Dynamic (or) Absolute viscosity in "centi Poise".
1.	45 $^\circ$	450	116.618	98.367	0.843.
2.	55 $^\circ$	370	95.736	80.131	0.837.
3.	65 $^\circ$	310	80.046	66.478	0.830.

Model calculation:-

1. Kinematic viscosity $KV = (A - B/t)$ centistokes.

where $A = 0.26$ } constant.
 $B = 172$

t = Time taken in seconds.

2. Absolute viscosity $= (KV \times \text{density})$ poise/ Ns/m^2 .

where density of oil at room temperature is 0.84 (or) $0.85 \text{ gm}/\text{cm}^3$.

PART-A. Exp: 2

Density of oil $\rho_t = \rho_r - 0.00065 (T - T_r)$.

i. Kinematic viscosity $KV = (At - B/t)$ centi Stokes.

$$i) KV = (10.26 \times 450) - 172/450$$

$$= 117 - 0.382$$

$$= 116.618 \text{ centi Stokes}$$

$$ii) KV = (10.26 \times 370) - 172/370$$

$$= 96.2 - 0.464$$

$$= 95.736 \text{ centi Stokes}$$

$$iii) KV = (10.26 \times 310) - 172/310$$

$$= 80.6 - 0.554$$

$$= 80.046 \text{ centi Stokes}$$

ii) Density of oil $\rho_t = \rho_r - 0.00065 (T - T_r)$.

$$i) \rho_t = 0.85 - 0.00065 (45 - 35)$$

$$= 0.85 - (6.5 \times 10^{-3})$$

$$= 0.8435 \text{ gm/cm}^3$$

$$ii) \rho_t = 0.85 - 0.00065 (55 - 35)$$

$$= 0.85 - 0.013$$

$$= 0.837 \text{ gm/cm}^3$$

$$iii) \rho_t = 0.85 - 0.00065 (65 - 35)$$

$$= 0.85 - 0.0195$$

$$= 0.8305 \text{ gm/cm}^3$$

PART-A Expt. 2

iii) Absolute viscosity = $\kappa v \times \text{density}$.

$$\begin{aligned} \text{i)} &= \kappa v \times \text{density} \\ &= 116.618 \times 0.8435 \\ &= 98.3672 \text{ Poise} \end{aligned}$$

$$\begin{aligned} \text{ii)} &= 95.736 \times 0.837 \\ &= 80.1310 \text{ centi Poise.} \end{aligned}$$

$$\begin{aligned} \text{iii)} &= 80.046 \times 0.8305 \\ &= 66.4782 \text{ centi Poise.} \end{aligned}$$

PART-A EXP. 3

Observation and Tabulation:-

1) Room temperature $T_R = 35^\circ\text{C}$.

2) Density of oil at room temperature = 0.85 gm/cm^3 .

S. No.	Temperature of oil $^\circ\text{C}$.	Time taken to fill 60 cc of oil 'sec'	Kinematic viscosity in 'cent Stokes'	Density of oil	Dynamic (or) Absolute viscosity 'centipoise'
1.	50°C	320	71.711	0.840	60.231
2.	60°C	275	61.441	0.833	51.180
3.	70°C	245	54.575	0.827	45.133

Model calculation:-

1. Kinematic viscosity $\mu_v = (At - B/t)$ centi Stokes.

where $A = 0.226$ and $B = 19.5$ upto 38°C .

$A = 0.226$ and $B = 135$ above 38°C .

t = Time taken fill the flask in seconds.

2. Absolute viscosity = (Kinematic viscosity $\times$ density) / Poise (or) Ns/m^2 .

3. Density of oil $\rho_t = \rho_r - 0.00065 \cdot (T - T_R)$

PART-A EXP. 3

i) Kinematic viscosity $KV = (At - B/t)$ centi stokes.

$$\begin{aligned} \text{i) } KV &= (0.226 \times 320) - (195/320) \\ &= 72.32 - 0.609 \\ &= 71.711 \text{ centi stokes} \end{aligned}$$

$$\begin{aligned} \text{ii) } KV &= (0.226 \times 275) - (195/275) \\ &= 62.15 - 0.709 \\ &= 61.441 \text{ centi stokes} \end{aligned}$$

$$\begin{aligned} \text{iii) } KV &= (0.226 \times 245) - (195/245) \\ &= 55.37 - 0.795 \\ &= 54.575 \text{ centi stokes} \end{aligned}$$

ii) Density of oil $\rho_t = \rho_g - 0.00065 (T - T_R)$.

$$\begin{aligned} \text{i) } \rho_t &= 0.85 - 0.00065 (50 - 35) \\ &= 0.85 - 9.75 \times 10^{-3} \\ &= 0.840 \text{ gm/cm}^3 \end{aligned}$$

$$\begin{aligned} \text{ii) } \rho_t &= 0.85 - 0.00065 (60 - 35) \\ &= 0.85 - 0.01625 \\ &= 0.833 \text{ gm/cm}^3 \end{aligned}$$

$$\begin{aligned} \text{iii) } \rho_t &= 0.85 - 0.00065 (70 - 35) \\ &= 0.85 - 0.02275 \\ &= 0.827 \text{ gm/cm}^3 \end{aligned}$$

Part-A Exp. 2

3) Absolute viscosity = $K_v \times \text{density}$.

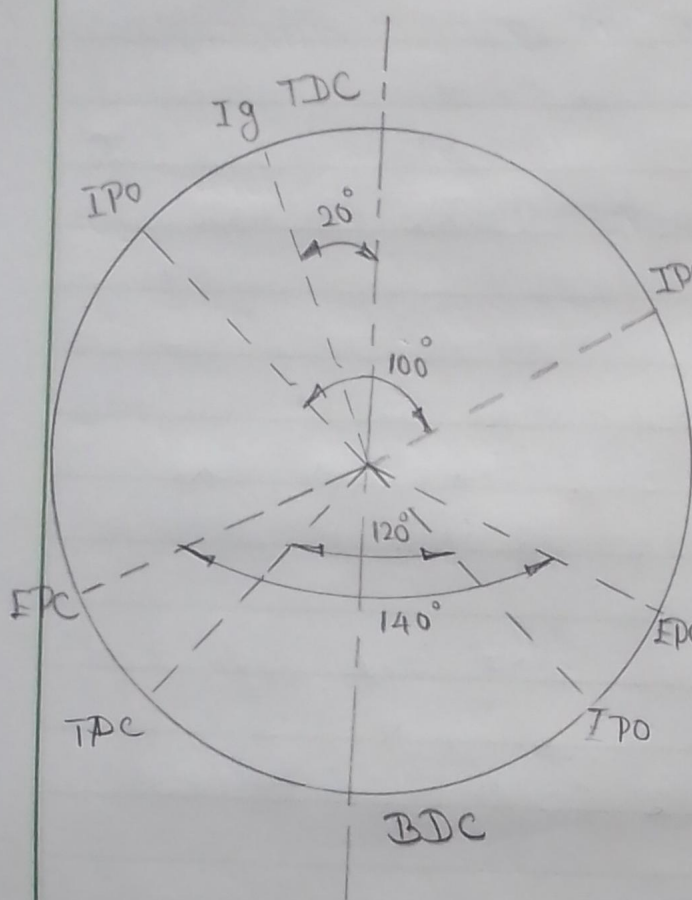
$$\begin{aligned}\text{i)} &= K_v \times \text{density} \\ &= 71.711 \times 0.840 \\ &= 60.237 \text{ centi Poise.}\end{aligned}$$

$$\begin{aligned}\text{ii)} &= K_v \times \text{density} \\ &= 61.441 \times 0.823 \\ &= 51.180 \text{ centi Poise.}\end{aligned}$$

$$\begin{aligned}\text{iii)} &= K_v \times \text{density} \\ &= 54.575 \times 0.827 \\ &= 45.133 \text{ centi Poise.}\end{aligned}$$

PART A EXP: 4

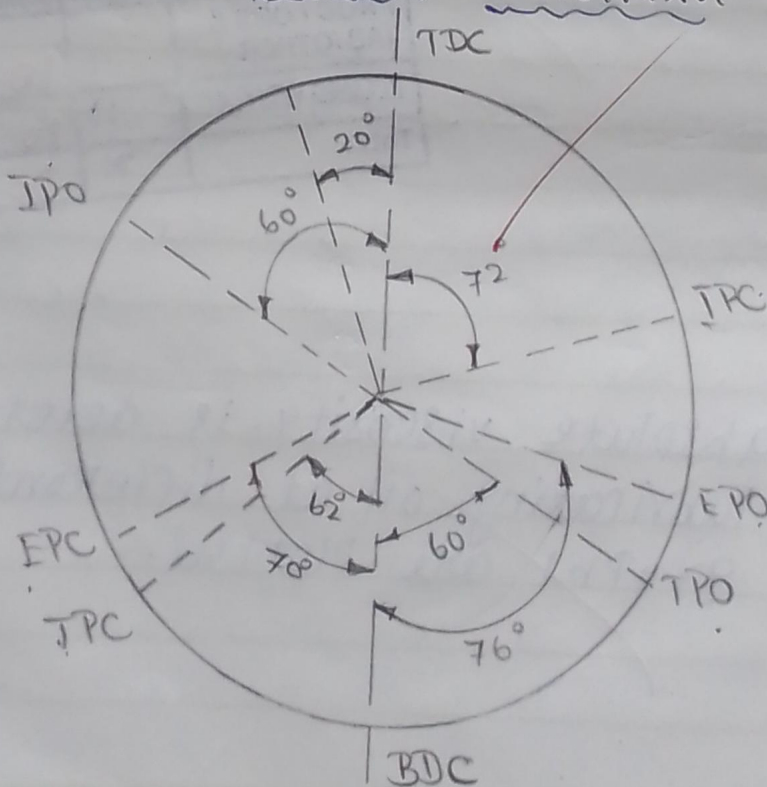
THEORETICAL PORT TIMING DIAGRAM OF 2 STROKE PETROL ENGINE.



IPO - Inlet Port opens.
 IPC - Inlet Port close.
 TPO - Transfer Port open.
 TPC - Transfer Port closes.
 Ig - Ignition.
 EPO - Exhaust Port opens.
 EPC - Exhaust Port close.

IPO - IPC : Suction.
 IPO - TPO : Crankcase compression.
 TPO - TPC : Transfer.
 TPC - Ig : Compression.
 Ig - TPO : Expansion.
 EPO - EPC : Exhaust.

PORT TIMING DIAGRAM.



observation and tabulation :-

- i) circumference of fly wheel = 490 mm
- ii) circumference distance in degree 360°

S. No.	Event	Before (or) After	Timing in	
			Distance in mm (x)	Angle in Degree
1.	TPO	Before BDC.	82 mm	60°
2.	TPC	After BDC.	85 mm	62°
3.	IPO	Before BDC.	104 mm	76°
4.	EPC	After BDC	95 mm	70°
5.	IPO	Before TDC.	83 mm	60°
6.	IPC	After TDC.	98 mm	72°

Model calculation:-

Angle of opening / closing of valve = $\frac{360^\circ}{\text{circumference of fly wheel.}} \times \text{distance measured from TDC (or) BDC.}$

$$\begin{aligned} \text{i) TPO} &= \frac{360^\circ \times 82}{490} \\ &= 60^\circ \end{aligned}$$

$$\begin{aligned} \text{ii) TPC} &= \frac{360}{490} \times 85 \\ &= 62^\circ \end{aligned}$$

PART-A Ex. 4

$$\text{iii) EPO} = \frac{360^\circ}{490} \times 104$$
$$= 76^\circ$$

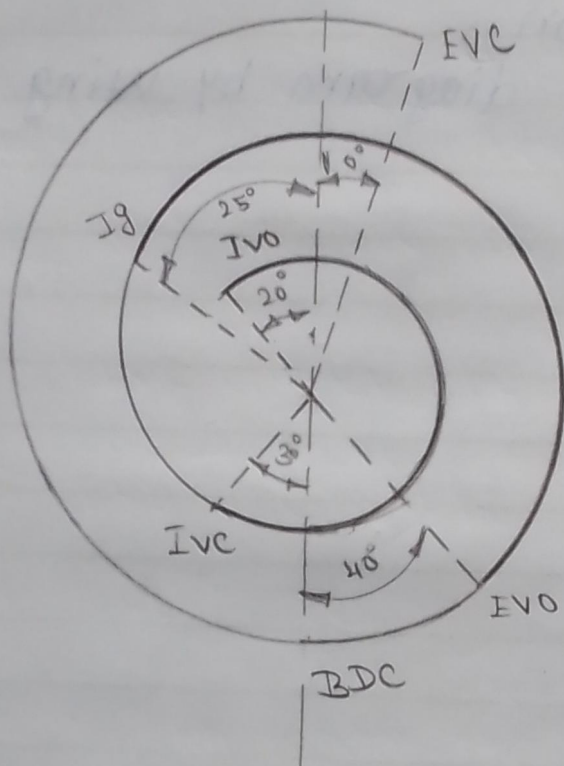
$$\text{iv) EPC} = \frac{360^\circ}{490} \times 95$$
$$= 70^\circ$$

$$\text{v) IPO} = \frac{360^\circ}{490} \times 83$$
$$= 60^\circ$$

$$\text{vi) IPC} = \frac{360^\circ}{490} \times 98$$
$$= 72^\circ$$

PART-A EXP'S

THEORETICAL VALVE TIMING DIAGRAM OF A STRAIGHT PETROL ENGINE.



IVO - Inlet valve open

Igc - Inlet valve close

Igc - Ignition.

EVO - Exhaust valve open.

EVC - Exhaust valve closes.

IVO - Igc - Suction.

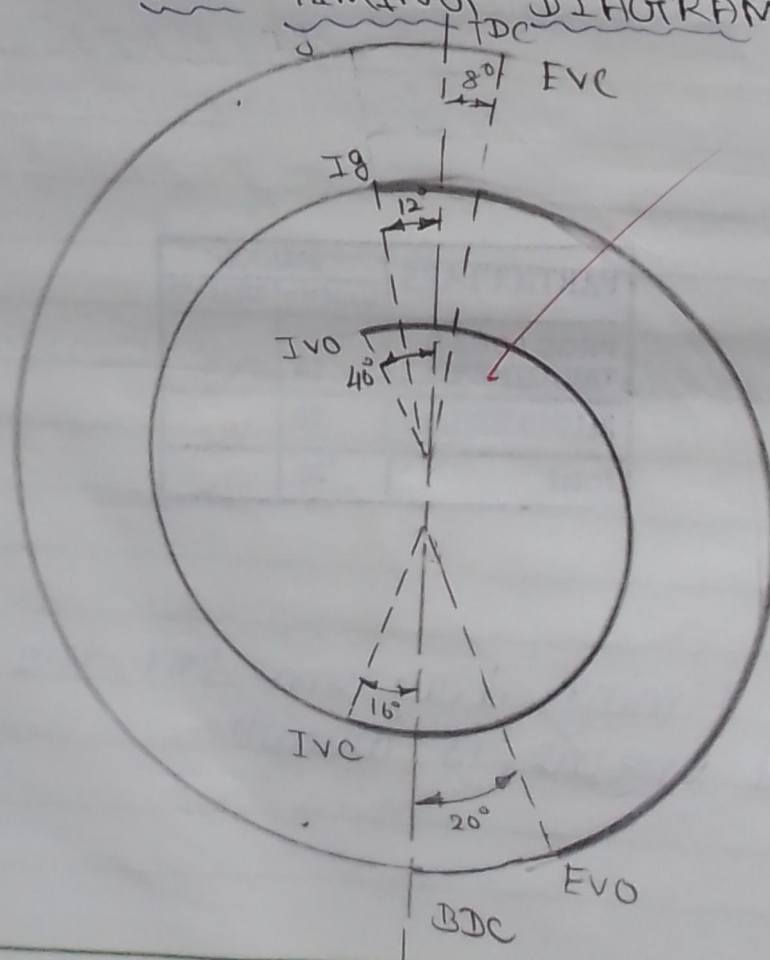
Igc - Igc : Compression.

Igc - EVO : Expansion.

EVO - EVC : Exhaust.

IVO - Igc : valve overlap.

PORT TIMING DIAGRAM.



PART A EXP'S

Observation and tabulation:-

circumference of fly wheel = $\frac{450 \text{ mm}}{1} = 360^\circ$

S. No.	Event	Before (or) After	Timing in	
			Distance in mm	Angle in Degree
1.	I.V.O	Before TDC	50	40°
2.	I.V.C	After BDC	20	16°
3.	E.V.O	Before BDC	25	20°
4.	E.V.C	After TDC	10	8°
5.	Ignition	Before TDC	15	12°

Model calculation:-

Angle of opening/closing of valve = $\frac{360^\circ}{\text{circumference of flywheel}} \times \text{distance for BDC (or) TDC}$
with respect to TDC (or) BDC

$$1) \text{ I.V.O} = \frac{360}{450} \times 50 = 40^\circ$$

$$2) \text{ Ignition} = \frac{360}{450} \times 15$$

$$ii) \text{ I.V.C} = \frac{360}{450} \times 20 = 16^\circ$$

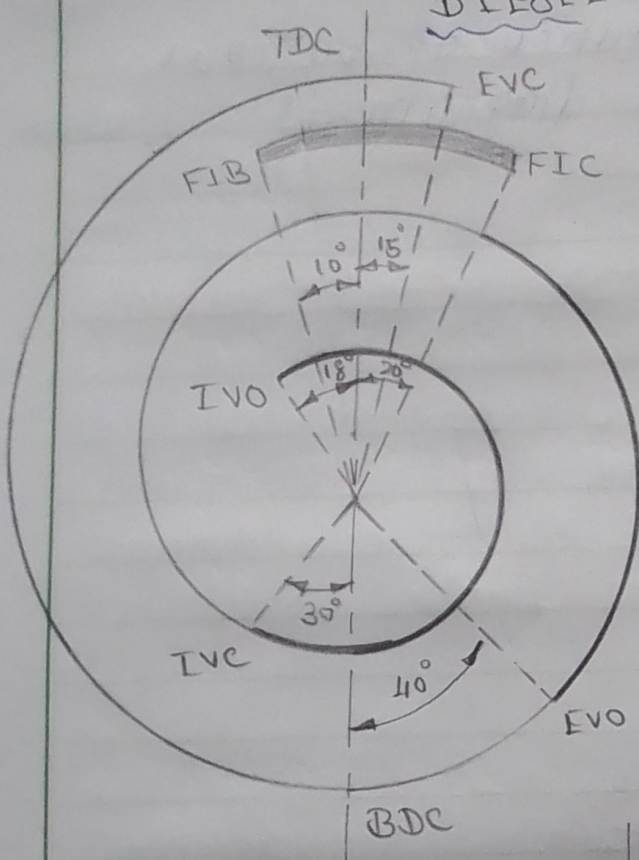
$$= 12^\circ$$

$$iii) \text{ E.V.O} = \frac{360}{450} \times 25 = 20^\circ$$

$$iv) \text{ E.V.C} = \frac{360}{450} \times 10 = 8^\circ$$

PART-A EXPI6

THEORETICAL VALVE TIMING DIAGRAM OF 4 STROKE DIESEL ENGINE.



IVO - Inlet valve open
 IVC - Inlet valve close.
 FIB - Fuel Injection begin
 FIC - Fuel Injection close.
 EVO - Exhaust valve open.
 EVC - Exhaust valve close.

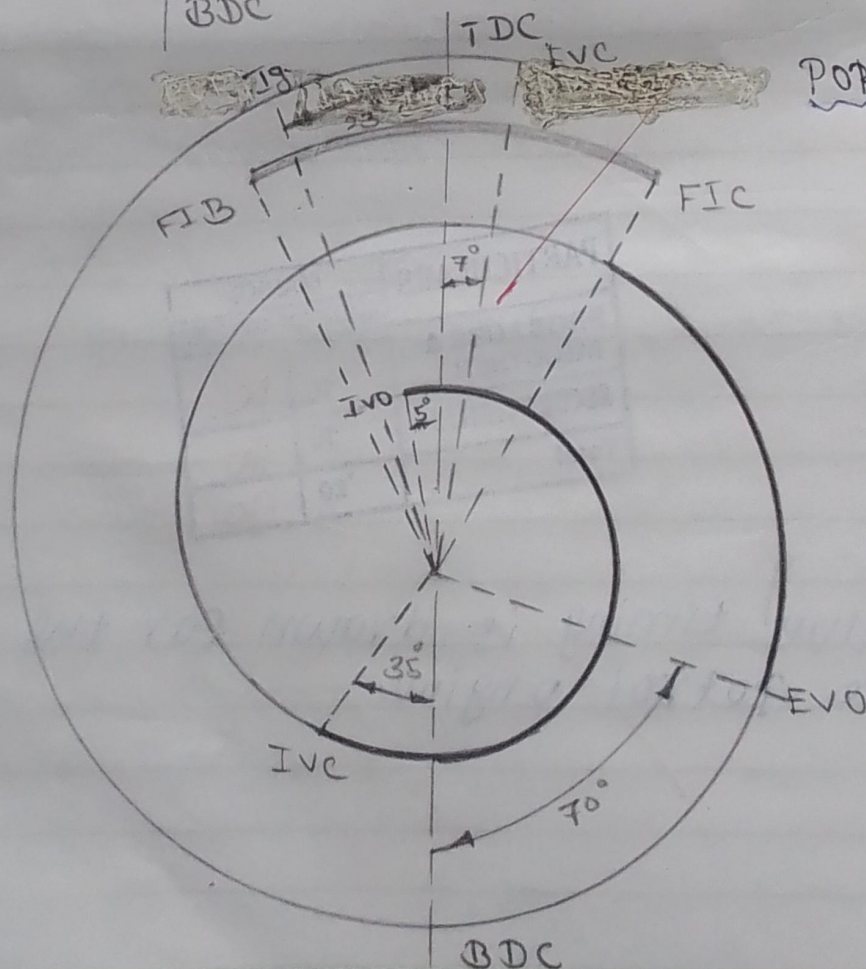
IVO - IVC : suction.

IVC - FIB : compression.

FIB - FIC : Fuel Injection.

FIC - EVO : EXPANSION.

EVO - EVC : Exhaust.



PORT TIMING DIAGRAM.

Part A

Exp 16

Observation and Tabulation:-

circumference of fly wheel = 1540 mm = 360°

S. No.	Event	Before (or) After.	Timing in	
			Distance in mm	Angle in degrees
1.	I.V.O	Before TDC	20	5°
2.	I.V.C	After BDC.	150	35°
3.	E.V.O	Before BDC	90	70°
4.	E.V.C	After TDC.	30	7°
5.	Ignition	Before TDC.	100	23°

Model calculation:-

Angle of opening / closing of valve = $\frac{360^\circ}{\text{circumference of flywheel}} \times \text{distance from TDC (or) BDC}$
with respect to TDC (or) BDC

$$\begin{aligned} \text{i) IVO} &= \frac{360}{1540} \times 20 \\ &= 4.5^\circ \end{aligned}$$

$$\begin{aligned} \text{ii) IVC} &= \frac{360}{1540} \times 150 \\ &= 35.1^\circ \end{aligned}$$

$$\text{III) EVO} = \frac{360}{1540} \times 90$$
$$= 70^\circ$$

$$\text{iv) EVC} = \frac{360}{1540} \times 30$$
$$= 7^\circ$$

$$\text{v) Ignition} = \frac{360}{1540} \times 100$$
$$= 23^\circ$$